# Development and Testing of a High Cycle Life 30 A-h Sealed AgO-Zn Battery

Technical Memorandum 33-536

## R. S. Bogner

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JET PROPULSION LABORATORY

CALIFORNIA INSTITUTE OF TECHNOLOGY

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## PREFACE

The work described in this report was performed by the Guidance and Control Division of the Jet Propulsion Laboratory.

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The Phase II battery testing was performed by the Naval Ammunition Depot Quality Evaluation Laboratory Department, Crane, Indiana, on JPL Work Request DPR WO-5150.

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## ABSTRACT

A two-phase program was initiated to investigate design parameters and new technology to develop an improved AgO-Zn battery. The basic performance goal was 100 charge/discharge cycles (22 h/2 h) at 50% depth of discharge following a six-month period of charged stand at room temperature (25 ±4°C). Phase I, cell evaluation, involved testing 70 cells in fivecell groups. The major design variables were active material ratios, electrolyte concentrations, separator systems, and negative plate shape. Phase I testing showed that cycle life could be improved 10% to 20% by using greater ratios of zinc to silver oxide and higher electrolyte concentrations. Wedge-shaped negatives increased cycle life by nearly 100%. The FSC separator proved superior to RAI 2291 separators for cycle life; however, test results were complicated by the cell pack tightness, a variable not originally planned to be introduced into the test. Phase II battery evaluation, which was initiated before the Phase I results were known completely, involved evaluation of six designs as 19-cell batteries. Phase II testing was done at NAD Crane, Indiana. Only one battery exceeded 100 cycles following nine months charged stand. That battery, containing FSC separators, gave 204 cycles at 50% DOD before the first cell failed. Unfortunately, the wedge-shaped negative was not evaluated in Phase II. Phase II and Phase I failures were due to loss of negative plate capacity caused by negative plate erosion.

#### I. INTRODUCTION

Future planetary exploration missions contemplated by NASA/JPL impose increased stand-life and cycle-life requirements that cannot be reliably met by the sealed silver oxide-zinc battery designs used on past spacecraft.

The silver oxide-zinc system is desirable over other systems for space applications because of its high energy density, high rate capability, low magnetic properties, and relatively low capacity loss on stand. JPL is engaged in development programs to improve the stand-life and cycle-life capabilities of the system. The development program discussed herein was initiated primarily to attempt to meet the design requirements for a Mariner Mars spacecraft.

ESB, Inc., was selected as the contractor for the development effort. A two-phase program was initiated to evaluate various design features, to assess the capability of these designs as cells and batteries, and to meet the performance requirement consisting of a six-month open-circuit charged stand at room temperature followed by 100, 24-h cycles at 50% depth-of-discharge (DOD). Other requirements included:

- (1) Recharge within 24 h.
- (2) Operation in a space vacuum.
- (3) Operation in the temperature range of 50 to 100°F.
- (4) Meet the environmental requirements set forth in JPL Specification TS 500437 Rev. B (Mariner Mars 1971).

The Phase I effort of the program was to evaluate several design parameters and testing methods, in five- to ten-cell groups. The Phase II effort was to test the best designs from Phase I in 19-cell batteries. Phase II was initiated before Phase I was complete; however, initial performance data from Phase I cells assisted in the design of the Phase II cells.

#### II. PHASE I CELL DESIGNS

Initially, cell design considerations were to include, but not necessarily be limited to, the investigation and analysis of the following:

- (1) Separator configuration on both positive and negative electrodes.
- (2) A means of preventing growth of zinc over or out of its separator compartment.
- (3) New types of separators.
- (4) Cell characteristics as a function of electrode thickness during charge and discharge.
- (5) Numbers of layers of separator material.
- (6) Electrolyte concentration.
- (7) Concentration of negative plate additives.
- (8) Electrolyte quantity.
- (9) Active material ratio.
- (10) Maximum overcharge capability.
- (11) Constant current versus constant potential charge methods.
- (12) Methods of accelerated testing.

Because of funding limitations, it was not possible to include all of the variables listed and certain compromises were made.

The design variables investigated in the Phase I cells were:

- (1) ZnO:Ag weight ratios, 1.4:1 and 1.2:1.
- (2) KOH electrolyte concentration, 45% and 41%, both 90% saturated with ZnO.
- (3) Negative plate shape, standard and wedge.
- (4) Type of semipermeable membrane, RAI 2291, fibrous sausage casing (FSC), irradiated EM 476I (polypropylene), and EM 470 (Dynel).
- (5) Type of absorber.

(6) Separator combination and electrode wrapped, i.e., negative vs positive wrap combination.

To evaluate these variables, ESB set up a test matrix on 70 cells consisting of seven basic designs. Each basic design group was divided into two five-cell groups, each also with a different design parameter. Table 1 lists the experimental design test matrix. The separator systems used in the cells consisted of combinations of two "absorbers" and two membranes as shown in Table 1. The "absorber" is a relatively inert material placed next to the positive electrode to help prevent oxidation of the membrane and to absorb electrolyte. The two types, both made by Kendall Mills, were Dynel (EM 470) and irradiated polypropylene (EM 4761). The semipermeable membranes were (FSC) fibrous sausage casing, made by the Visking Division of Union Carbide, and (RAI 2291) irradiated polyethylene grafted with methacrylic acid, made by RAI, Inc.

Table 1 also indicates which electrode was wrapped and how combinations of the separator membrane were positioned in the cell. For example, Design Group 3 had four layers of RAI 2291 on the positive electrode followed by two layers of FSC on the positive electrode; the absorber was dynel. Design Group 6 had three layers of RAI 2291 on the positive electrode and four layers of RAI 2291 on the negative electrode; the absorber was polypropylene. The electrolyte and ZnO:Ag weight ratio columns show the number of cells of each design group that contain the listed variable.

A nine-cell group of Mariner Mars 1969 cell designs was also tested for comparison with the new designs and is shown at the bottom of Table 1. The Mariner Mars 1969 cells contained one layer of polypropylene EM 4761 and six layers of cellophane 193 PUDO around the positive electrode.

Initially, the pack tightness (or pressure) of all seven cell designs was to be the same based on a common set of design equations. The cell element (plate and separator stack) thickness was calculated based on the design thickness of the positive and negative plates and the measured wet thickness of the separator system used in each design. The wet thickness of each separator system was determined by measurement with a Randall-Stickney gauge after 120 h soak in 45% KOH. The resultant measurements are shown in Fig. 1. Pack tightness was calculated based on the wet thickness of the separator system at 1.64 N/cm<sup>2</sup>. At this pressure it was thought that the

major wrinkles in the separators would be smoothed out and still allow some free electrolyte to remain between the layers.

One cell of each design was fabricated early to verify the design tolerances. The element designs that contained two or more layers of FSC could be inserted into the cell jar easily. The element designs that did not contain FSC could not be inserted in the cell jar without damaging and compressing the cell element. The reason for this is that the FSC expands approximately 100% when wet while the RAI material expands 10% or less and generally contains many fine wrinkles. Since the separator systems were of different thicknesses, plastic shims were used to take up excess volume in the cell jar. The original pack pressures were reduced by decreasing shim thicknesses. Consequently, another design variable, pack tightness, was introduced somewhat randomly into the test. The final calculated pack pressures are listed in Table 1.

Design features common to all cells in both Phase I and II are listed in Table 2. The electrolyte was added to the cells under vacuum to remove air pockets. The cells were completely filled (flooded) and soaked for 72 h. After a formation charge, the cells were inverted to drain off the excess electrolyte. After draining, the cell fill holes were sealed. According to past design practice by ESB, the proper quantity of electrolyte is thus retained in the cell. However, this method of electrolyte adjustment is subject to question when using new types of separator material and needs further investigation. Table 3 lists the quantity of electrolyte retained in each cell, which was obtained by weighing the cells before and after draining.

### III. PHASE I TESTING AND RESULTS

The cells were formation charged at 1.55 mA/cm<sup>2</sup> (1.53 A) for an input of 47 A-h (0.38 A-h/g of silver). The cells were discharged at 15 A to 1.25 V cutoff. The minimum discharge capacity was 0.313 A-h/g of silver for all designs except Group 5 which gave only 0.123 A-h/g of silver (15.1 A-h). For the second discharge of Design 5 cells, the discharge rate was reduced from 15 A to 8 A, but there was no appreciable increase in capacity. It was concluded that the Design 5 cell pack was too tight; however, it is also possible that there was not enough electrolyte in the cells.

The cell groups were given three to four additional cycles using twostep charge and discharge rates to attempt to obtain uniform performance from the cells. However, there was still considerable capacity variation among cells of the same design. The maximum variation was about 10 A-h. The reasons for the wide variations in a given design are not understood. Tables 4 through 10 give the detailed charge and discharge rates and the capacities of each cell and design group.

After approximately four months charged stand the cells were discharged, charged, and placed on a 24-h cycle regime at 50% depth of discharge (DOD). The cycle consisted of 2 h of discharge and a 22-h charge at a constant potential with a current limit of 1.5 A.

The cell groups were discharged through a resistance adjusted to give an average current of 7.50 A over 2 h (15 A-h). An Esterline-Angus 24-point recorder was used to record cell group current and cell group voltages. At 25- to 30-cycle intervals, each cell group was discharged until the first cell reached 1.30 V (100% DOD), to measure total capacity as a function of cycle life. When a cell in the group could not support the 50% DOD it was considered failed. The charge potential of 1.94 ±0.01 V/cell was used for the first 50 to 65 cycles (not all design groups were on the same cycle number) and was raised to 1.96 ±0.01 V thereafter because it appeared the cells were not accepting proper charge as noted by falling end-of-discharge voltage and rising end-of-charge current, primarily on Design Group 3. When the charge potential was increased, recovery was noted by the increase in end-of-discharge voltage. This was particularly evident on Design Group 3. There was no appreciable change in Design Group 2; however, Design

Group 7 started to develop leaks, apparently from high pressures, and this group was considered failed at 55 to 57 cycles. Figure 2 summaries the cycle life of the Phase I cells based on the first cell failure. With the exceptions of Designs 5 and 7 as noted above, the remaining design groups failed from loss of capacity due to negative electrode erosion. None of the cells failed by shorting through the separator system.

The eight-cell row assembly of Mariner Mars 1969 cells tested at the same time and cycled under the same routine failed at 32 cycles by shorting through the separator. The cells were also near failure due to negative electrode erosion because most of the active material was observed to be in the lower 25% of the plate grid.

Two design groups gave significantly better cycle results than the others. Design Group 1, with the wedge-shaped negative, gave 226 cycles compared with its control with standard negatives which gave 136 cycles. Design Group 2 cells gave 213 and 251 cycles for each of the 5 cell groups, suggesting that FSC is a much better separator. The results from groups 1 and 2 suggest that a significant improvement might be achieved by combining the wedge negative and the FSC separator.

The effect of electrolyte concentration is seen in Design Groups 2 and 3. The cell groups containing 45% KOH gave 10 to 20% higher cycle life than those with 41% KOH.

The increase in material ratio showed an improvement in cycle life of 10% to 20% as can be noted from the results obtained from Groups 4 and 6.

Since failures were due to loss of capacity and not shorts it is difficult to attribute this failure mode specifically to the separator system. It is felt that some other design factors or test factors not readily evident contributed to the results. Perhaps cell pack tightness played a role in the failure. The reasons for failure will be discussed further at the end of Phase II test results.

Impedance measurements were made on the cells with a model 502 Keithly milliohmmeter before formation, after formation, and after stand. The significance of the measurements at present is not completely understood, but the results were recorded for future reference. Generally, the impedances before formation ranged from about 40 to 60 m $\Omega$  and after

formation were about 50% less. After the stand period the values increased about ten fold. No attempt has been made to correlate the impedance measurements with cell performance.

## IV. PHASE II CELL DESIGNS

Due to schedule limitations, it became necessary to initiate Phase II of the program before Phase I cycling tests were completed. Consequently, one of the most promising designs, the wedge-shaped negative, was omitted from the Phase II effort.

The remaining six designs (Groups 2 through 7) were repeated in the Phase II effort with some modifications. The modifications were as follows:

- (1) 43% KOH electrolyte saturated with ZnO was used in all cells.
- (2) ZnO-to-Ag weight ratio was 1.5:1 in all cells.
- (3) An additional layer of polypropylene (EM 476I) was added to Design Group 6 around the negative plate.
- (4) Formation charge: 1.09 mA/cm<sup>2</sup> to 0.36 to 0.38 A-h/g of silver, or 2.1 V/cell.
  - Top off after seal at 1.09 mA/cm<sup>2</sup> to  $^{\circ}$ . 38 to 0.42 A-h/g of silver, or 1.97 V/cell.
- (5) Electrolyte was added to bring low cells up to the group mean value.
- (6) Calculated pack pressures were reduced in Designs 4 and 5 by about 50%.
- (7) Cell elements were designed to occupy full thickness of cell jar instead of using shims as in Phase I.

Table 11 summarizes the design group variables and shows the mean quantity of electrolyte in each group. Table 12 shows the quantity of electrolyte in each cell.

Since the cell elements were designed to occupy the full thickness of the cell jar, the design groups contained different numbers of plates. Plates were added to those designs that contained RAI 2291 separators because the thickness of this material is less than that of FSC, as noted previously in Phase I designs and shown in Fig. 1. The number of electrodes and their thicknesses are also recorded in Table 11.

#### V. PHASE II TESTING AND RESULTS

After the formation charge as noted above, the cells were discharged at a current density of 8.06 mA/cm<sup>2</sup> or approximately the C/4 rate (C is the rated capacity of the cell) to 1.30 V. This was followed by an additional charge/discharge cycle and recharge. The charge and discharge parameters and results of these three cycles are given in detail in Tables 13 through 19.

Following the third charge cycle, the cells were shipped to the Naval Ammunition Depot, Crane, Indiana, (NAD-Crane) for stand and cycle-life test. From the time the cells were first activated and during the test, they were in a room temperature environment estimated to be 25 ±4 °C except during shipment from ESB to NAD Crane. After a stand period of approximately nine months, the cells were tested with a phenolphthalene solution for electrolyte leaks in preparation for cycling tests. No leaks were detected. Cells were monitored for leakage throughout the test, but leakage was not considered as criteria for the failure in these tests.

Before the cells were placed on cycle tests they were given two capacity check cycles at the C/4 discharge rate to 1.30 V per cell. The charge was in two steps as follows: 1.09 mA/cm<sup>2</sup> of positive plate area to 2.00  $\pm 0.01$  V/cell followed by a charge of 0.62 mA/cm<sup>2</sup> of positive plate area to 1.98  $\pm 0.01$  V/cell.

After the capacity check cycles, the cells were placed on an automatic cycle regime as six 19-cell batteries. The cycle regime was the same as used in Phase I tests: Discharge at C/4 rate for 2 h, recharge at a constant potential of 1.94 ±0.01 V/cell with a current limit of 1.50 A for 22 h. Individual battery and cell voltage measurements were recorded periodically on each cycle. Every 25 cycles the batteries were given a 100% discharge (until the first cell in the battery reached 1.30 V) to measure capacity degradation as a function of cycle life. If any cell in a battery dropped to 1.30 V during the 50% DOD cycles, the cell was removed from the battery and cycling was continued after adjusting the battery charge potential. The battery was considered to have failed when the first cell could not support the 50% DOD.

Figure 3 compares the capacities of each design before stand, after stand, and the second capacity check after stand. The spread in capacity and the average capacity are also shown in Fig. 3. It is seen that all design groups lost capacity during stand that was not recoverable on the second capacity check after stand. Design Group 3 produced the most consistent data and Group 4 gave the most inconsistent results with a capacity spread of over 20 A-h. Large spreads in capacity indicate there are uncontrolled factors in cell fabrication. The cycle data was analyzed to ascertain if the low capacity cell was the first cell to fail on cycling. The results are shown in Table 20 where the low cell of each capacity check cycle at 25-cycle intervals was recorded. The low cell was consistently low only in Design Group 5.

The results of the cycling test are summarized in Figs. 4, 5, and 6. Figure 4 shows the capacity available from each group as measured on the lowest cell at 25-cycle intervals. Only Design Group 2, containing four layers of FSC, passed the 100-cycle requirement. It gave 204 cycles before the first cell dropped below 50% of its rated capacity.

Design Groups 6 and 4, containing only the RAI separator material, failed first at 39 and 52 cycles, respectively. Design Groups 3, 5, and 7, containing combinations of RAI 2291 and FSC separators, failed at 84, 90, and 99 cycles. All failures were due to loss of capacity caused by the erosion of the negative active material.

A measure of the electrical performance of each battery is shown in Fig. 5, where the average cell potential at the end of 2 h of discharge on the cycling test is shown as a function of cycle. Design Group 2 with the FSC separator shows the best electrical performance. Design Groups 3, 5, and 6 with combinations of RAI 2291 and FSC separators are next, all with similar performance; Groups 4 and 6, containing only RAI 2291, again show the worst performance.

Figure 6 shows the rate of failure of the cells in each group. From this data it is seen that the failure rate is fairly uniform. Design Group 7 had an early failure. The autopsy and analysis of the failed cell revealed it was unusually dry and the failure was attributed to a manufacturing defect. Representative samples of failed cells from each Design Group were autopsied for failure analysis. It was observed that the negative plate material was

concentrated on the lower portion of the plate grid and, in most instances, the edges of the lower portion of the plate were also devoid of active material. This type of failure is not strictly attributable to the separator system, or is not what might be termed a first-order failure caused by the separator. Shorting failures would be a first-order failure attributable to the separator system.

The data tends to lead one to the conclusion that the early failures of the design groups containing the RAI 2291 separator membrane were probably associated with the cell pack pressure. The pack pressure was less in Design Groups 4 and 6 than in the design group containing the FSC separator (Group 2) or in groups containing combinations of RAI 2291 and FSC (Groups 3, 5, and 7). The cycle results show the negative electrode to have eroded more rapidly and failed sooner in design groups with low pack pressures than in the design groups with high pack pressures. On the other hand, it is pointed out that the Design Group 5 cells in Phase I with pack pressures equal to the pressure of Design Group 2 with FSC separators failed to perform properly in that they delivered only about one-half their rated capacity.

From these results it is concluded that further testing and analysis are needed to elucidate the pertinent design factors affecting performance when using new types of separator membranes. A better knowledge of the effects and interactions of pack pressure (also better methods of measurement), electrolyte volume, and absorber are required. Since the RAI 2291 membrane and similar membranes absorb very little electrolyte and swell very little in comparison to cellulosic-type membranes it is possible that a thicker, more absorbent "absorber" might be beneficial. The nature of the movement or erosion of the negative material is also more complicated than indicated by the above discussion and is probably due to several effects. If the problem of negative plate erosion were solved, it would be a major advancement in the state-of-the-art in silver oxide-zinc battery technology.

The data do not indicate whether it is preferable to wrap the separator around the negative or positive electrode, nor do the data indicate if it is beneficial to use one absorber in preference to the other (EM 476I or EM 470). A more rigorous analysis of the data might show some subtle differences.

#### VI. CONCLUSIONS

Test results from six 19-cell batteries indicate that silver-zinc batteries can be designed to meet the requirements of spaceflight when such requirements call for high cycle life (more than 100 24-h cycles at 50% depth-of-discharge) after a period (at least 6 months) on charged open-circuit stand. Although the designs were not subjected to environmental tests nor were the performance parameters tested over an expected operational temperature range, the comparable results represent an improvement in cycle life over that of the Mariner Mars 1969 design by a factor of six.

The design parameters that effected an improvement in cycle life were:

- (1) Increased electrolyte concentration.
- (2) Increased negative-to-positive material ratio.
- (3) Wedge-shaped negative plates.
- (4) Fibrous sausage casing separators.

The wedge-shaped negative plate design was evaluated in cells with only the RAI 2291 separators. The wedge-shaped negative should be evaluated with the FSC separator. From the results obtained with the wedge negatives in conjunction with RAI separators (100% improvement), it is estimated the combination of wedge negative plates and FSC separators should produce a battery capable of 300 cycles.

From this work it could not be determined if it is better to wrap the separator membrane around the negative or positive plate. Of the two absorbers tested (EM 476I and EM 470), there was no indication that one was better than the other.

The results obtained from the use of RAI 2291 separator membranes were disappointing. Future development work should investigate the effects of the interactions of pack pressures, electrolyte volume, and thicker, more absorbent absorbers.

Since cell failures in this investigation were due to capacity loss and not shorting, the optimum number of layers of separators was not determined. Future work should optimize the number of layers of separators for a given life to prevent shorting.

Table 1. Phase I cell design matrix (10 cells/design)

DE SI GN NUMBER		ATOR <sup>a</sup> STEM	ELECTR	1	, -	WT RATIO	PACK PRESSURE
NOMBER	ABSORBER	MEMBRANE	41% KOH	45% KOH	1.2:1	1.4:1	N/cm <sup>2</sup>
1	P/P	6 2291-	-	10	10b	-	0.08-1.64b
2	DYNEL	4 FSC -	5	5	10	-	3.29
3	DYNEL	4 2291+ 2 FSC +	5	5	10	-	1.64
4	P/P	6 2291-	10	-	5	5	0.08-0.49
5	DYNEL	4 2291- 2 FSC -	5	5	10	-	3.29
6	P/P	3 2291+ 4 2291-	10	-	5	5	0.49
7	DYNEL	2 FSC - 4 2291-	5	5	10	-	0.49

MARINER 69 P/P

6 CELLO +

0.76:1

<sup>a</sup> ORDER OF PLATE WRAP IS AS LISTED
<sup>b</sup> 5 CELLS CONTAINED WEDGE NEGATIVES

- NEGATIVE WRAP

+ POSITIVE WRAP

Table 2. Phase I and II common design features

NEGATIVE	PLATE		%
	COMPOSITION:	ZnO HgO TEFLON	90 3 7
	PROCESS: DENSITY: GRID:	DRY POWE 2.75 g/cm <sup>3</sup> SILVER	DER-SINTERED 2 - 2/0 D
POSITIVE		51 <b>2</b> 12	
	COMPOSITION: DENSITY: PROCESS: GRID:	100% Ag 4.24 g/cm <sup>3</sup> PROPRIET/ SILVER	
CELL JAR A	ND COVER	ABS	(CYCOLAC T)
		T W H	3.88 cm 8.72 cm 9.45 cm
SEALANT	EPOCAST 31/0	CA9216	

Table 3. Electrolyte quantities in Phase I cells

				Adjuste	ed Elect	rolyte(	Quantity	
Design No.	Design Variation	Units		Ce	11 Numl	per		$\overline{\mathbf{x}}_{5}$
			1	2	3	4	5	5
1	Flat Plates	gm cc	121 79.2	118 77.2	119 77.8	118 77.2	118 77.2	119 77.8
1	Wedge Plates	gm cc	149 97.5	149 97.5	150 98.0	151 98.6	151 98.6	150 98.0
2	45% KOH	gm cc	163 106	164 107	161 105	166 108	161 109	163 106
2	41% KOH	gm cc	161 109	162 110	159 108	159 108	162 110	161 109
	45% KOH	gm cc	141 92.1	143 93.6	143 93.6	143 93.6	144 94.1	143 93.5
3	41% KOH	gm cc	139 94.6	139 94.6	139 94.6	146 99.3	141 96.1	141 96.0
	1.4:1	gm cc	110 75.0	119 81.0	121 82.3	122 83.0	119 81.0	118 80.3
4	1.2:1	gm cc	111 75.5	109 74.2	109 74.2	109 74.2	109 74.2	109 74.2
	45% KOH	gm cc	142 92.8	147 96.2	149 97.4	151 98.7	148 96.8	147 96.1
5	41% KOH	gm cc	143 97.3	147 100.0	142 96.6	143 97.3	144 98.0	144 98.0
	1.4:1	gm cc	122 83.1	114 77.6	119 81.0	119 81.0	121 82.6	119 81.0
6	1.2:1	gm cc	114 77.6	113 76.8	106 72.2	109 74.1	106 72.2	110 75.0

Table 4. Charge and discharge rates, Design Group 1

Design 1 (45% KOH)		Fl	at Nega	tive Pla	tes			Conto	ured N	egative	Plates	
Cell S/N	6	40	41	42	43	$\bar{x}_5$	8	44	45	46	47	$\bar{x}_5$
-Wrap, 6 RAI; 1 EM-476I(+)												
Cycle 1												
• Charge (formation), AH 1.53 amps to Input	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2
<ul> <li>AC Impedance before charge, mohms after charge, mohms</li> </ul>	39 20	34 15	36 13	34 15	39 22	36 17	48 18	51 32	51 32	52 15	55 18	51 23
Discharge, AH     @ 15 amps to 1.25V (1st cell)     Midpoint voltage, volts	41.8 1.46	41.8 1.47	41.8 1.47	41.8	41.8 1.47	41.8	40.5 1.45	40.6* 1.46	40.6* 1.45	40.6* 1.47	40.6*	40.6 1.46
Cycle 2  • Charge, AH Step 1 @ 1.53 amps to 1.99V Step 2 @ 0.6 amp to Input Total	45.6	<b>47</b> . 9	46.2	45.6	47.9		44.0	** 39.8	** 39.8	** 39.8	** 37.8 2.0 39.8	
Discharge, AH     @ 15 amps to 1.25V/cell     Midpoint voltage, volts	42.8 1.45	46.8 1.46	46.3 1.48	42.6 1.45	42.7 1.45	45.2 1.46	(* 8 ar	dural C nps to l 53 amps	. 30 vol		cell)	
Cycle 3						İ						
<ul> <li>Charge, AH</li> <li>Step 1 @ 1.53 amps to 1.97V</li> <li>Step 2 @ 0.6 amp to input</li> <li>Total</li> </ul>	22.6 14.0 36.6	43.1	46.2	32.9 4.8 37.7	38.2 4.8 43.0	 						
<ul> <li>Top off Charge, AH</li> <li>6 amp to 1.97V/cell</li> <li>Total</li> </ul>										1.7 39.9	1.7 37.8	
• Discharge, AH Step I @ 15 amps to 1.25 V (1st cell) Step II @ 5 amps to 1.25 V/cell Total Midpoint Voltage, Volts, Step I	21.3 14.4 35.7 1.44	21.3 20.5 41.8 1.45	21.3 23.1 44.4 1.44	21.3 14.4 35.7 1.45	21.3 21.3 42.6 1.44	40.0 1.44	20.0 0.9 20.9 1.44	21.3 17.5 38.8 1.44	21.3 19.1 40.4 1.44	38. 7 3. 4 42. 1 1. 47	38.7 1.9 40.6 1.48	 1.45
Cycle 4  Charge, AH Step I @ 1.5 amps to 1.97V/cell Step II @ 0.6 amp to 1.97V/cell	37.9	37.9	36.9	36.2	36.2		45.7	36.2	36.2	36.9	36.9	
Total  Discharge, AH										12.2 49.1	11.4 48.3	
Step I @ 1.5 amps to 1.25V/1st cell	34.2	34. 2	34.2	34.2	34.2		34.2	34.2	34.2	44.8	40.5	
Step II @ 0.5 amp to 1.25V/cell Total Midpoint Voltage, Volts, Step 1	$\frac{2.9}{37.1}$ 1.45	$\frac{2.8}{37.0}$ 1.46	$\frac{2.1}{36.3}$ 1.46	$\frac{1.6}{35.8}$ 1.46	$\frac{1.2}{35.4}$ 1.46	36.3 1.46	10.8 45.0 1.45	$\frac{2.2}{36.4}$ 1.44	2.4 36.6 1.44	 44.8 1.46	40.5 1.46	40.7 1.45
Cycle 5  Charge, AH Step I @ 1.5 amps to 1.97V/cell Step II @ 0.6 amp to 1.97V/cell Total	47.3 4.0 51.3	50.6 2.5 53.1	51.8 2.5 54.3	49.3 4.6 53.9	47.3 3.7 51.0	49.3 3.5 52.7	47.3 6.3 53.6	44.2 6.9 51.1	44.9 6.3 51.2	38.8 7.7 46.5	38. 2 7. 7 45. 9	42.7 7.0 49.7

Table 5. Charge and discharge rates, Design Group 2

Design 2			45%	кон					41%	кон		
S/N of Cell	ı	9	10	11	12	$\bar{x}_5$	13	14	15	16	17	$\vec{x}_5$
+ Wrap: 1 EM-470, 4 FSC												
Cycle 1							:					
Charge (formation), AH     1.23 amps to Input	47.0	47.0	47.0	47.0	47.0	47.0	47.0	47.0	47.0	47.0	47.0	47.0
AC Impedance before charge, mohms after charge, mohms	62 90	74 80	62 90	58 80	32 70	58 82	56 60	60 60	63 50	60 50	56 60	59 56
Discharge, AH     @ 15 amps to 1.25V (1st cell)     midpoint voltage, volts	38.5 1.47	38.5 1.47	38.5 1.47	38.5 1.46	38.5 1.47	 1.47	38.5 1.48	38.5 1.48	38.5 1.48	38.5 1.48	38.5 1.48	1.48
Cycle 2												
<ul> <li>Charge, AH         Step 1 @ 1.23 amps to 1.99V         Step 2 @ 0.70 amp to 2.00V         Total</li> </ul>	39.6 39.6	43.6  43.6	39.6  39.6	20.5 26.2 46.7	37.4  37.4	36. 1 41. 4	41.0	41.0	38.0	33.8	40.5	38.9
<ul> <li>Discharge, AH</li> <li>@ 15 amps to 1.25V/Cell</li> <li>midpoint voltage, volts</li> </ul>	41.2 1.46	45.6 1.50	23.5 1.42	43.7 1.51	33.0 1.40	37.4	43.1 1.48	42.5 1.48	34.8 (Jar burst)	32.8 1.48	42.1 1.48	39.1
Cycle 3		!										
• Charge, AH Step 1 @ 1.23 amps to 1.97V Step 2 @ 0.6 amp to 1.97V Total	38.4  38.4	36.3  36.3	38.5	16.8 13.1 29.9	36.3  36.3		39.2	39.2		34.4	39.4	
• Top off charge, AH .6 amps to 1.97V/cell Total	17.8	18.0 54.3	18.0 56.5	178 477	18.6 54.9	53.9	18.6 57.8	17.0 56.2	22.2 56.6	19.1 58.5	57.3	
<ul> <li>Discharge, AH*         Step I @ 12 amps to 1.25V (1st Cell)         Step II @ 4 amps to 1.25V/Cell         Total         Midpoint voltage, volts, Step I</li> </ul>	42.3 4.8 47.1 1.49	42.3 5.3 47.6 1.49	42.3 6.3 48.6 1.49	42.3 1.4 43.7 1.49	42.3 3.7 46.0 1.49	42.3 4.3 46.6 1.49	42.3 8.3 50.6 1.49	42.3 7.1 49.4 1.49	42.3 6.5 48.8 1.49	42.3 9.1 51.4 1.49	42.3 7.7 50.0 1.49	
Cycle 4												
Charge, AH Step I @ .9 amps to 1.97V/cell Step II @ .6 amps to 1.97V/cell Total	33.1 11.1 44.2	39.8 2.2 42.0	38.6 4.0 42.6	39.8 3.5 43.3	33.1 11.5 44.6	36.9 6.4 43.3	39.8 5.9 45.7	39.8 5.4 45.2	37.0 4.0 41.0	39.8 5.9 45.7	39.1 5.3 44.4	
AC Impedance, mohms after Cycle 4 charge	47	58	63	65	59	58	57	64	27	42	48	
Cell pack pressure: 80 ounces/in <sup>2</sup> Plate wrapped: Positive Order of Wrap, pos. to neg.: 1 EM470, 4 FSC Zn0 to silver weight ratio 1.2:1												

<sup>(\*)</sup> Step I 0.10 amp/in<sup>2</sup> Step II 0.33 amp/in<sup>2</sup>

Table 6. Charge and discharge rates, Design Group 3

Design 3			45%	кон					41%	кон		
Cell S/N	2	18	19	20 .	21	$\bar{x}_5$	22	23	24	25	26	$\bar{x}_5$
+ Wrap: 1 EM-470, 4 RAI, 2 FSC												
Cycle 1												
Charge (formation, AH     1.53 amps to Input	47.1	47.1	47.1	47.1	47.1	47.1	47.1	47.1	47.1	47. 1	47.1	47.1
AC Impedance     before charge, mohms     after charge, mohms	57 19	53 14	56 20	56 19	70 14	58 17	56 16	59 14	57 12	57 20	56 12	57 15
Discharge, AH     @ 15 amps to 1.25V (1st cell)     midpoint voltage, volts	40.1	40.1 1.46	40.1 1.45	40.1 1.45	40.1 1.46	40.1 1.45	40.1 1.46	40.1 1.46	40.1 1.46	40.1 1.46	40.1 1.47	40.1 1.46
Cycle 2												
<ul> <li>Charge, AH</li> <li>Step 1 @ 1.53 amps to 1.99V</li> <li>Step 2 @ 0.70 amp to 2.00V</li> <li>Total</li> </ul>	16.6 23.4 40.0	20.1 24.2 44.3	33.7 5.1 38.8	19.3 27.6 46.9	38.5  38.5	39.7	37.0 7.0 44.0	36.2 4.4 40.6	39.2 39.2	38.5	38.6	 40. Ž
<ul> <li>Discharge, AH</li> <li>@ 8 amps to 1.40V/cell midpoint voltage, volts</li> </ul>	40.3	43.7 1.50	38.5 1.50	43.7 1.50	36.4 1.43	40.5	43.7 1.51	39.8 1.51	41.8 1.51	36.0* 1.45	37.6* 1.45	39.8
Cycle 3												
• Charge, AH Step 1 @ 1.53 amps to 1.97V Step 2 @ 0.6 amp to 1.97V Total	20.0 12.1 32.1	20. 0 4. 1 24. 1	20.0 12.1 32.1	20.0 12.1 32.1	13.0 <u>(Jar</u> B	urst)	20.0 10.3 30.3	20.0 <u>8.6</u> 28.6	20.0 15.7 35.7	32.9  32.9	36.4  36.4	32.8
<ul> <li>Top off Charge         0.6 amp to 1.97V/cell         Total</li> </ul>	8.8 40.9	14. 0 38. 1	13.8 45.9	8.7 40.8		13.2 43.5	17.8 46.4	11.6 47.3	13.7 46.6	13.2 49.6		
Discharge, AH     Step I @ 15 amps to 1.25V/(ist cell)     Step II @ 5 amps to 1.25V/cell     Total     Midpoint Voltage, Volts Step I	39.0 3.9 42.9 1.47	39. 0 3. 4 42. 4 1. 46	39.0 <u>8.5</u> 47.5 1.46	39.0 6.0 45.0 1.46	$   \begin{array}{r}     39.0 \\     \underline{6.0} \\     44.4 \\     1.46   \end{array} $	43.0 5.4 48.6 1.48	43.0 5.6 46.4 1.46	43.0 3.4 47.3 1.46	43.0 4.3 44.8 1.46	43.0 1.8 44.8 1.46	43.0 3.4 46.4 1.46	
Cycle 4		}										
• Charge, AH Step I @ 1.1 amps to 1.97V/cell Step II @ 0.6 amp to 1.97V/cell Total	39.8 3.3 42.1	34.6 11.8 46.4	34.6 2.4 37.0	34.6 11.8 46.4	35.9 7.3 43.2	34.8 3.0 37.8	34.8 <u>9.6</u> 44.4	34.8 10.8 45.6	34.8 10.0 44.8	34.8 12.0 46.8	34.8 9.0 43.8	

Table 7. Charge and discharge, rates, Design Group 4

Design 4 (41% KOH)		Zn0: A	kg Weig	ht Ratio	= 1.4:1	l		Zn0: A	Ag Weig	ht Ratio	= 1.2:	
Cell S/N	3	27	28	29 .	30	$\bar{x}_5$	52	53	54	55	56	$\bar{x}_5$
- Wrap, 6 RAI; 1 EM-476I (+)												
Cycle 1												
• Charge (formation), AH 1.53 amps to Input	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2
<ul> <li>AC Impedance before charge, mohms after charge, mohms</li> </ul>	39 20	39 24	37 18	39 36	39 17	39 23	36 16	36 23	37 16	38 23	41 12	38 18
• Discharge, AH @ 15 amps to 1.25V (1st cell) midpoint voltage, volts	41.8 1.46	41.8 1.47	41.8 1.46	41.8 1.47	41.8 1.48	41.8 1.47	40.6* 1.50	40.6* 1.49				
Cycle 2												
• Charge, AH Step 1 @ 1.53 amps to 1.99V	47.9	47.9	48.0	47.5	47.5	47.8	(*)	l 8 amp	rate to	1.30V,	l lst cel	1)
Discharge, AH     @ 15 amps to 1.25V/cell     midpoint voltage, volts	44.3 1.45	42.4 1.45	45.6 1.45	48. 2 1. 46	47.9 1.47	45.7 1.46						
Cycle 3												
• Charge, AH					İ	:						
Step 1 @ 1.53 amps to 1.97V Step 2 @ 0.6 amp to Input Total	$\frac{22.6}{14.0}$ $\frac{14.0}{36.6}$	36.4 4.8 41.2	43.1  43.1	43.8	44.6	41.9						
• Top off charge 0.6 amp to 1.97V/cell Total	12.7 49.3	6. 1 47. 3	6.1 49.2	5.3 49.1	5.3 49.9	7.0 48.9	6.9 44.4	9.0 45.5	9.0 47.0	9.0 46.7	11.4 46.4	9.1 46.0
Discharge, AH     Step I @ 15 amps to 1.25V (1st cell)     Step II @ 5 amps to 1.25V/cell     Total	44.5 4.1 48.6	44.5 1.4 45.9	44.5 2.8 47.3	44.5 2.9 47.4	44.5 3.7 48.2	44.5 3.0 47.5	45.3	47.5 	47.5	47.5 	46. 2 	46.8
Midpoint Voltage, Volts, Step I	1.48	1.49	1.48	1.48	1.50	1.49	1.52	1.51	1.51	1.50	1.50	1.51
Cycle 4  • Charge, AH Step I, @ 1.5 amps to 1.97V/cell Step II @ 0.6 amp to 1.97V/cell Total	33.2 11.2 44.4	33. 2 9. 5 42. 7	33.2 10.9 44.1	33. 2 10. 4 43. 6	33.2 9.7 42.9	33. 2 10. 3 43. 5	41.7 3.9 45.6	39.4 3.3 42.7	41.0 3.3 44.3	39.5 3.9 43.4	39.5 3.9 43.4	40.2 3.6 43.8

Table 8. Charge and discharge rates, Design Group 5

Design 5			45%	кон					41%	кон	,	
Cell S/N	4	31	32	33	34	<b>x</b> <sub>5</sub>	35	36	37	38	39	$\overline{X}_5$
(4 RAI/2 FSC/1 EM-470/(+) - Wrap)												
Cycle 1												
<ul> <li>Charge (formation), AH</li> <li>1.53 amps to Input</li> </ul>	47.2	47. 2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2
<ul> <li>AC Impedance before charge, mohms after charge, mohms</li> </ul>	45 23	39 21	44 25	47 16	49 20	45 21	50 22	46 25	48 19	45 18	48 17	47 20
Discharge, AH     @ 15 amps to 1.25V (1st cell)     midpoint voltage, volts	15.1 1.35	15. 1 1. 42	15.1	15.1 1.42	15.1 1.42	15.1 1.40	15.1 1.42	15.1 1.43	15.1 1.44	15.1 1.43	15.1 1.43	15.1 1.43
Cycle 2												
• Charge, AH Step 1 @ 1.53 amps to 1.99V	26.4	28.4	21.4	21.3	19.2	23.3	21.8	21.4	21.4	21.1	22.3	21.6
<ul> <li>Discharge, AH</li> <li>@ 8 amps to 1.25 V/cell</li> <li>midpoint voltage, volts</li> </ul>	27.7 1.46	28. 2 1. 48	28.0 1.46	24. 2 1. 47	20.4 1.48	25.7 1.47	21.3 1.48	23.7 1.46	21.7 1.46	24.0 1.48	24.0 1.47	22.9 1.47
Cycle 3												
• Charge, AH Step 1 @ 1.53 amps to 1.97V Step 2 @ 0.6 amp to Input Total	13.8	18.3 4.8 23.1	17.7 4.8 22.5	17.7 4.8 22.5	14. 2 4. 8 19. 0	20.2	17.6 4.8 22.4	14. 4 4. 8 19. 2	16.7 4.8 21.5	17.2 4.8 22.0	17.2 4.8 22.0	21.4
• Top off charge, AH . 6 amps to 2.03 max. volts/cell Total	14.4 28.2	8.01 31.1	8.01 30.5	8.01 30.5	8.01 27.0	31.5	8.01 30.4	8.01 27.2	8.01 29.5	8.01 30.0	8.01 30.0	<del>2-</del> <del>29. 4</del>
<ul> <li>Discharge, AH         Step I @ 15 amps to 1.25V (1st cell)         Step II @ 5 amps to 1.25V/Cell         Total</li> </ul>	16.2 5.4 21.6	18.8 10.8 29.6	18.8 11.5 30.3	18.8 -7.5 26.3	18.8 <u>9.1</u> 27.9	18.3 8.9 27.1	18.8 10.8 29.6	18.8 11.9 30.7	18.8 <u>9.4</u> 28.2	18.8 <u>9.6</u> 28.4	16.2 12.3 28.5	18.3 10.8 29.1
Midpoint voltage, volts, Step I	1.41	1.43	1.42	1.40	1.42	1.42	1.43	1.42	1.42	1.43	1.42	1.42
Cycle 4												
• Charge, AH Step I @ 1.53 amps to 1.97V/cell Step II @ .6 amps to 1.97V/cell Total	19.6 4.9 24.5	20.0 6.7 26.7	20.0 6.9 26.9	21.6 6.9 28.5	21.6 2.9 24.5	20.6 6.4 26.2	23.2 4.9 28.1	20.0 <u>4.4</u> 24.4	22.6 4.0 26.6	22.6 6.4 29.0	22.6 4.7 27.3	22.2 4.8 27.0
Cell pack pressure: 80 ounces/in <sup>2</sup> Plate wrapped: negative Order of wrap: Positive to Negative: 1 EM470, 2 FSC, 4 RAI2291 Zn0 to Ag weight ratio: 1.2:1												

Table 9. Charge and discharge rates, Design Group 6

Design 6 (41% KOH)		Zn0/A	g Weigh	t Ratio	= 1.4:1			Zn0/A	g Weigh	t Ratio	= 1.2:1	
Cell S/N	5	48	49	50	51	<b>x</b> <sub>5</sub>	7	57	58	59	60	$\bar{x}_5$
(7 RAI/"Z" +, 1EM-476I, "U" -												
Cycle 1				!								
Charge (formation, AH     1.53 amps to Input	47.2	47. 2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2	47.2
<ul> <li>AC Impedance before charge, mohms after charge, mohms</li> </ul>	39 26	43 36	40 15	41 40	38 32	40 30	39 20	54 61	42 28	39 46	43 16	43 34
<ul> <li>Discharge, AH</li> <li>@ 8 amps to 1.30V (1st cell)</li> <li>midpoint voltage, volts</li> </ul>	40.6 1.46	40.6 1.46	40.6 1.47	40.6	40.6 1.48	40.6 1.47	40.6 1.45	40.6 1.48	40.6 1.48	40.6 1.47	40.6 1.45	40.6
Cycle 2												
• Charge, AH 1.53 amps	42.4	39.8	39.8	39.8	39.8		42.4	39.8	39.8	39.8	39.8	
<ul> <li>Discharge, AH         Step I @ 15 amps to 1.25V (1st cell)         Midpoint Voltage, Volts</li> </ul>	21.9	44. 7 1. 43	43.2 1.44	37. 2 1. 43	32.5 1.45	35.9 1.43	15.8 1.38	37.1 1.44	36.7 1.43	44.5 1.45	38. 2 1. 42	34. 2 1. 42
Cycle 3		:										
<ul> <li>Charge, AH         Step I @ 1.53 amps to 1.97V/cell         Step II @ 0.6 amp to 1.97V/cell         Total</li> </ul>	22.6	33. 2 9. 8 43. 0	33.2 6.9 40.1	33.2 8.6 41.8	33.2 10.1 43.3		19.4	35.7	36.5	33.3	$   \begin{array}{r}     33.2 \\     \hline     8.0 \\     \hline     41.2   \end{array} $	
• Top Off Charge, 0.6 amp to 1.97 + .03 -0	19.9	2.1	2.5	1.7	1.7		17.1	8.8	8.8	8.8	2.6	•
volt/cell Total	42.5	45.1	42.6	43.5	45.0	43.7	36.5	44.5	45.3	42.1	35.8	40.8
• Discharge, AH Step I @ 15 amps to 1.25V 1st cell Step II @ 5 amps to 1.25V/cell	35.7	35.7 2.6	35.7	35.7	35.7	35.7 2.2	42.8	47.5	46.2	46.2	46.8	45.9
Total Midpoint Voltage, Volts, Step I	37.2 1.46	38. 3 1. 44	37.8 1.45	38.3 1.44	37.9 1.45	37.9 1.45	1.46	1.45	1.45	1.45	1.44	1.45
Cycle 4												
Charge, AH Step I @ 1.5 amps to 1.97V/cell Step II @ 0.6 amp to 1.97V/cell Total	40.0 4.1 44.1	37.0 7.2 44.2	37.0 7.2 44.2	31.4 5.0 36.4	31.4 3.5 34.9	35.4 5.4 40.8	41.0 4.0 45.0	35.3 7.3 42.6	35.3 7.4 42.7	41.0 8.0 49.0	38.2 7.5 45.7	38. 2 6. 8 45. 0

Table 10. Charge and discharge rates, Design Group 7

		41% KOH	КОН					45% KOH	ОН		·
Test Parameter and S/N 61	29	63	64	65	$\overline{\mathbf{x}}_{5}$	99	29	89	69	70	XI S
Cycle 1											
• Charge (formation), AH 48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
Before formation, mohms  After formation, mohms  Discharge Au	53	44	50	45 29	49 27	51	63	59 33	53	50 39	55 36
14 amps to 1.30V lst cell 32.7 Midpoint Voltage 1.47	32.7	32.7	32.7	32.7	32.7	37.1 1.48	37. 1 1. 47	37.1	37.1 1.48	37.1 1.47	37.1 1.48
Cycle 2											
• Charge, AH Step I at 0.97 amp to 1.97V 1st cell 35.7	35.	35.7	35.7	35.7	35.7	34.9	34.9	34.0	34 0	24 0	24.0
Step II at 0.6 amp to 1.97V/cell 5.1 Total 40.8	39.6	2.0	39.3	1.4	38.2	14.5	1.4	25.7	14.5	4.5	9.1
			) 1	•		H		-	+ - / +	# · ^ #	4 <b>4.</b> 0
		4 rv	34.5 8.3	34.5	34.5	31.9	31.9	31.9	31.9	31.9	31.9
Total 42.0 Midpoint Voltage at 14 amps 1.45	44.2	39.9	1.45	35.8	40.1	39.8	35.2	36.9	41.8	41.9	39.1
_						1		2	2	) 1	) •
• Charge, AH Step I at 0, 97 amp to 1, 97 V 1st cell 30 0	30	30	30.0	0	0		0		2		
	_	4.4	2.6	5.4. 5.4.	4.0	1.8	2.8	5. 4. 0	24.8 2.2	54.8 2.7	24.8
~		34.4	32.6	34.4	34.0	36.6	37.6	40.2	39.0	35.0	37.7

Cell nominal capacity 28 AH based on 0.25 AH/gram silver. Date of activation: 11/3/69 - Date on charged stand: 11/21/69. (1) NOTES:

Table 11. Phase II design group construction features

Electrolyte	ave/cell m cc	118	102	93	106	98	101
Elect	ave/ gm	176	153	139	158	147	152
Rated*	Capacity Ah	25	28	31	28	28	28
s, mm	Half Negative	8.64	8.64	None Used	8.64	None Used	8.64
Plate Thickness, mm	Full Negative	17	17	17	17	17	17
Plate	Positive	6.35	6.35	6.35	6.35	6.35	6.35
ıtes	Half Negative	2	2	0	7	0	2
Number of Plates	Full Negative	2	8	11	8	10	8
Nun	Positive	∞	6	10	6	6	6
Pack	Pressure N/cm <sup>2</sup>	3.29	1.64	0.25	1.64	0.49	1.64
	System	1EM470 + 4FSC +	1EM470 + 2FSC + 4RAI2291 +	1EM476 I - 6RAI -	1EM470 - 2FSC - 4RAI2291 -	7RAI2291 <sup>b</sup> 2EM476 I	1EM470 + 4RAI2291 + 2FSC +
-	Design	2	3	4	ī.	9	7

 $^*$ Rated at 0.25 Ah/gm of Silver

<sup>&</sup>lt;sup>a</sup>Order of wrap is as listed: - Negative plate wrap, + positive plate wrap

<sup>&</sup>lt;sup>b</sup>Both electrodes wrapped: + EM4761, 3RAI 2291; - 4RAI2291, EM476I

Table 12. Phase II adjusted electrolyte quantities

Quantity KOH         GMS         CC         GMS         CC </th <th>Design No.</th> <th>7</th> <th></th> <th>3</th> <th></th> <th>4</th> <th></th> <th>5</th> <th></th> <th>9</th> <th></th> <th>•</th> <th>7</th>	Design No.	7		3		4		5		9		•	7
175   117   154   103   138   92.0   160   107   145   96.7   152   175   118   150   100   143   95.4   158   105   147   98.1   153   175   117   158   105   147   98.1   153   175   117   158   105   147   98.1   153   175   117   154   103   140   93.4   160   107   151   100   152   175   117   154   103   138   92.0   160   107   151   100   152   175   117   151   101   139   92.0   160   107   147   98.1   152   175   117   152   103   138   92.0   160   107   147   98.1   152   175   117   152   101   140   93.4   160   107   147   98.1   152   175   117   152   101   140   93.4   160   107   145   96.7   152   175   117   153   102   138   92.0   160   107   145   96.7   152   177   118   154   103   138   92.0   160   107   145   96.7   152   177   118   157   105   141   94.0   160   107   144   95.9   152   177   118   154   102   141   94.0   160   107   145   96.7   152   175   117   153   102   141   94.0   160   107   145   96.7   152   175   117   153   102   141   94.0   156   104   145   96.7   152   175   117   153   102   141   94.0   156   104   145   96.7   152   175   117   153   102   141   94.0   156   104   145   96.7   152   175   117   153   102   141   94.0   156   104   145   96.7   152   175   117   153   102   141   94.0   158   105   145   96.7   152   175   117   153   102   141   97.9   152   175   117   153   102   141   97.9   152   175   17	antity KOH	GMS	၁၁	GMS	၁၁	GMS	၁၁	GMS	သ	GMS	သ	GMS	၁၁
175         117         154         103         138         92.0         160         107         145         96.7         152           177         118         150         100         143         95.4         158         105         147         98.1         153           175         117         148         98.7         137         91.3         160         107         143         95.4         150         107         151         100         152           176         117         154         103         140         93.4         160         107         151         100         152           177         118         155         103         138         92.0         160         107         147         98.1         152           177         118         152         101         139         92.0         160         107         147         98.1         152           175         117         154         103         139         92.0         160         107         147         98.1         152           175         117         153         102         138         92.0         160         107         144 <td>ell No.</td> <td></td>	ell No.												
177         118         150         100         143         95.4         158         105         147         98.1         153           175         117         148         98.7         137         91.3         160         107         143         95.4         153           175         117         158         105         139         92.6         160         107         151         100         152           175         117         154         103         140         93.4         160         107         151         100         152           175         117         151         101         140         93.4         160         107         151         100         152           175         117         154         103         138         92.0         160         107         149         99.4         152           175         117         152         101         140         93.4         160         107         149         99.4         152           175         117         152         101         140         93.4         160         107         149         99.4         152           175	1	175	117	154	103	138	92.0	160	107	145	96.7	152	101
175         117         148         98.7         137         91.3         160         107         143         95.4         152           175         117         158         105         139         92.6         160         107         151         100         152           176         117         151         101         140         93.4         160         107         151         100         152           177         118         155         103         138         92.0         160         107         147         98.1         152           175         117         154         103         138         92.0         160         107         144         99.4         152           175         117         152         101         140         93.4         160         107         145         99.4         152           175         117         152         101         140         93.4         160         107         145         96.7         152           175         117         153         102         138         92.0         160         107         145         96.7         152           181	- 2	177	118	150	100	143	95.4	158	105	147	98.1	153	102
175         117         158         105         139         92.6         160         107         151         100         152           176         117         154         103         140         93.4         160         107         151         103         152           177         118         155         103         138         92.0         160         107         147         98.1         152           175         117         151         101         139         92.6         153         102         147         98.1         152           175         117         154         103         138         92.0         160         107         147         98.1         152           175         117         154         103         138         92.0         160         107         144         96.7         152           177         118         154         103         138         92.0         160         107         144         95.9         152           177         118         154         103         138         92.0         160         107         144         95.9         152           181	3	175	117	148	98.7	137	91.3	160	107	143	95.4	152	101
176         117         154         103         140         93.4         160         107         155         103         152           175         117         151         101         140         93.4         160         107         151         100         152           177         118         155         103         138         92.0         160         107         147         98.1         152           175         117         154         103         138         92.0         160         107         149         99.4         152           175         117         152         101         140         93.4         160         107         145         99.4         152           175         117         153         102         138         92.0         160         107         145         96.7         152           175         117         150         100         138         92.0         160         107         144         97.4         152           181         121         153         102         141         94.0         160         107         144         95.9         152           177	4	175	117	158	105	139	95.6	160	107	151	100	152	101
175         117         151         101         140         93.4         160         107         151         100         152           177         118         155         103         138         92.0         160         107         147         98.1         152           175         117         154         103         138         92.0         160         107         147         98.1         152           175         117         154         103         138         92.0         160         107         145         99.4         152           175         117         153         102         138         92.0         160         107         145         96.7         152           177         118         154         103         138         92.0         160         107         144         96.7         152           181         121         153         102         141         94.0         160         107         144         95.9         152           181         121         153         102         144         94.0         160         107         144         95.9         152           175	22	176	117	154	103	140	93.4	160	107	155	103	152	101
177         118         155         103         138         92.0         160         107         147         98.1         152           175         117         154         103         138         92.0         160         107         149         99.4         152           175         117         152         101         140         93.4         160         107         145         96.7         152           175         117         153         102         138         92.0         160         107         145         96.7         152           177         118         154         103         139         92.0         160         107         145         96.7         152           175         117         150         100         138         92.0         160         107         144         95.9         152           181         121         153         102         141         94.0         160         107         144         95.9         152           177         118         148         98.7         142         94.0         160         107         144         95.9         152           175 <td>9</td> <td>175</td> <td>117</td> <td>151</td> <td>101</td> <td>140</td> <td></td> <td>160</td> <td>107</td> <td>151</td> <td>100</td> <td>152</td> <td>101</td>	9	175	117	151	101	140		160	107	151	100	152	101
175     117     151     101     139     92.6     153     102     150     100     152       175     117     154     103     138     92.0     160     107     149     99.4     152       175     117     152     101     140     93.4     160     107     145     96.7     152       175     117     153     102     138     92.0     160     107     146     97.4     152       175     117     150     100     138     92.0     160     107     146     97.4     152       181     121     153     102     141     94.0     160     107     144     95.9     152       181     121     153     102     141     94.0     160     107     144     95.9     152       177     118     148     98.7     142     94.7     160     107     144     95.9     152       175     117     151     101     142     94.7     160     107     144     95.9     152       175     117     153     102     143     94.0     160     107     144     95.4     152 <t< td=""><td>2</td><td>177</td><td>118</td><td>155</td><td>103</td><td>138</td><td>92.0</td><td>160</td><td>107</td><td>147</td><td>98. 1</td><td>152</td><td>101</td></t<>	2	177	118	155	103	138	92.0	160	107	147	98. 1	152	101
175         117         154         103         138         92.0         160         107         149         99.4         152           175         117         152         101         140         93.4         160         107         145         96.7         152           175         117         153         102         138         92.0         160         107         145         96.7         152           177         118         154         103         139         92.0         160         107         146         97.4         152           181         121         150         100         138         92.0         160         107         144         97.4         152           181         121         153         102         141         94.0         160         107         144         95.9         152           177         118         148         98.7         142         94.7         160         107         144         95.9         152           175         117         151         101         142         94.7         160         107         144         95.4         152           175 <td>∞</td> <td>175</td> <td>117</td> <td>151</td> <td>101</td> <td>139</td> <td></td> <td>153</td> <td>102</td> <td>150</td> <td>100</td> <td>152</td> <td>101</td>	∞	175	117	151	101	139		153	102	150	100	152	101
175     117     152     101     140     93.4     160     107     145     96.7     152       175     117     153     102     138     92.0     160     107     145     96.7     152       177     118     154     103     139     92.6     156     104     147     98.1     152       175     117     150     100     138     92.0     160     107     146     97.4     152       181     121     153     102     141     94.0     160     107     144     95.9     152       177     118     148     98.7     142     94.7     160     107     144     95.9     152       175     117     151     101     142     94.7     160     107     149     99.4     152       175     117     153     102     138     92.0     160     107     149     99.4     152       175     117     153     102     141     94.0     158     105     145     96.7     152       175     117     153     102     141     94.0     156     104     145     96.7     - <tr< td=""><td>6</td><td>175</td><td>117</td><td>154</td><td>103</td><td>138</td><td></td><td>160</td><td>107</td><td>149</td><td>99.4</td><td>152</td><td>101</td></tr<>	6	175	117	154	103	138		160	107	149	99.4	152	101
175     117     153     102     138     92.0     160     107     145     96.7     152       177     118     154     103     139     92.6     156     104     147     98.1     152       175     117     150     100     138     92.0     160     107     146     97.4     152       181     121     153     102     141     94.0     160     107     144     95.9     152       177     118     148     98.7     142     94.7     160     107     144     95.9     152       175     117     151     101     142     94.7     160     107     149     99.4     152       175     117     153     102     138     92.0     160     107     149     99.4     152       175     117     153     102     141     94.0     158     105     145     96.7     152       175     117     153     102     141     94.0     156     104     145     96.7     152       175     117     151     101     136     90.7     156     104     145     96.7     - <tr< td=""><td>10</td><td>175</td><td>117</td><td>152</td><td>101</td><td>140</td><td></td><td>160</td><td>107</td><td>145</td><td>96.7</td><td>152</td><td>101</td></tr<>	10	175	117	152	101	140		160	107	145	96.7	152	101
177     118     154     103     139     92.6     156     104     147     98.1     152       175     117     150     100     138     92.0     160     107     146     97.4     152       181     121     153     102     141     94.0     160     107     144     95.9     152       177     118     148     98.7     142     94.7     160     107     144     95.9     152       175     117     151     101     142     94.7     160     107     146     97.4     152       175     117     153     102     138     92.0     160     107     149     99.4     152       175     117     153     102     141     94.0     158     105     145     96.7     152       175     117     151     101     136     90.7     156     104     145     96.7     -       175     117     155     103     136     90.7     156     104     145     96.7     -       175     117     155     102     139     92.0     150     106     146     97.4     -	11	175	117	153	102	138	95.0	160	107	145	7.96	152	101
175     117     150     100     138     92.0     160     107     146     97.4     152       181     121     153     102     141     94.0     160     107     147     98.1     158       177     118     148     98.7     142     94.0     160     107     144     95.9     152       175     117     151     101     142     94.7     160     107     146     97.4     152       175     117     153     102     138     92.0     160     107     149     99.4     152       175     117     153     102     141     94.0     158     105     145     96.7     152       175     117     151     101     136     90.7     156     104     145     96.7     -       175     117     155     103     136     90.7     156     104     145     96.7     -       176     118     157     105     138     92.0     150     100     146     97.4     -       176     118     153     102     139     92.0     150     106     147     97.9     152	12	177	118	154	103	139		156	104	147	98.1	152	101
181         121         153         102         141         94.0         160         107         147         98.1         158           177         118         157         105         141         94.0         160         107         144         95.9         152           177         118         148         98.7         142         94.7         160         107         144         95.9         152           175         117         151         101         142         94.7         158         105         146         97.4         152           175         117         153         102         141         94.0         158         105         149         99.4         152           175         117         151         101         136         90.7         156         104         145         96.7         -           175         117         155         103         136         90.7         156         104         145         96.7         -           175         117         155         105         138         92.0         150         104         145         96.7         -           178	13	175	117	150	100	138		160	107	146	97.4	152	101
177         118         157         105         141         94.0         160         107         144         95.9         152           177         118         148         98.7         142         94.7         160         107         145         96.7         152           175         117         151         101         142         94.7         158         105         146         97.4         152           175         117         153         102         141         94.0         158         105         149         99.4         152           175         117         151         101         136         90.7         156         104         145         96.7         -           175         117         155         103         136         90.7         156         104         145         96.7         -           175         117         155         103         136         90.7         156         104         145         96.7         -           178         119         157         105         138         92.0         150         100         146         97.4         -           176	14	181	121	153	102	141		160	107	147	98. 1	158	105
177     118     148     98.7     142     94.7     160     107     145     96.7     152       175     117     151     101     142     94.7     158     105     146     97.4     152       175     117     153     102     141     94.0     158     105     149     99.4     152       175     117     151     101     136     90.7     156     104     145     96.7     -       175     117     155     103     136     90.7     156     104     145     96.7     -       178     119     157     105     138     92.0     150     100     146     97.4     -       176     118     153     102     139     92.0     150     106     147     97.9     152	15	177	118	157	105	141	94.0	160	107	144	95.9	152	101
175     117     151     101     142     94.7     158     105     146     97.4     152       175     117     153     102     138     92.0     160     107     149     99.4     152       175     117     153     102     141     94.0     158     105     145     96.7     152       175     117     151     101     136     90.7     156     104     145     96.7     -       178     119     157     105     138     92.0     150     100     146     97.4     -       176     118     153     102     139     92.8     158     106     147     97.9     152	16	177	118	148	98.7	142	94.7	160	107	145	96.7	152	101
175     117     153     102     138     92.0     160     107     149     99.4     152       175     117     153     102     141     94.0     158     105     145     96.7     152       175     117     151     101     136     90.7     156     104     145     96.7     -       175     117     155     103     136     90.7     156     104     145     96.7     -       178     119     157     105     138     92.0     150     100     146     97.4     -       176     118     153     102     139     92.8     158     106     147     97.9     152	17	175	117	151	101	142	94.7	158	105	146	97.4	152	101
175     117     153     102     141     94.0     158     105     145     96.7     152       175     117     151     101     136     90.7     156     104     145     96.7     -       175     117     155     103     136     90.7     156     104     145     96.7     -       178     119     157     105     138     92.0     150     100     146     97.4     -       176     118     153     102     139     92.8     158     106     147     97.9     152	18	175	117	153	102	138		160	107	149	99.4	152	101
175     117     151     101     136     90.7     156     104     145     96.7     -       175     117     155     103     136     90.7     156     104     145     96.7     -       178     119     157     105     138     92.0     150     100     146     97.4     -       176     118     153     102     139     92.8     158     106     147     97.9     152	19	175	117	153	102	141		158	105	145	96.7	152	101
175     117     155     103     136     90.7     156     104     145     96.7     -       178     119     157     105     138     92.0     150     100     146     97.4     -       176     118     153     102     139     92.8     158     106     147     97.9     152	20	175	117	151	101	136	90.7	156	104	145	6.7	,	ı
178   119   157   105   138   92.0   150   100   146   97.4   -	21	175	117	155	103	136	90.7	156	104	145	7.96	ı	ı
176   118   153   102   139   92.8   158   106   147   97.9   152   1	22	178	119	157	105	138	95.0	150	100	146	97.4	,	
	×	176	118	153	102	139	95.8	158	901	147	6.76	152	101

Cycling performance of Phase II Design 2 cells Table 13.

Plate Wrapped: Positive; Order of Separation,	+ to -:	1EM470,	l	4FSC; Nominal Capacity:	nal Cap		25 AH				
Test Parameter and Cell S/N	1	2	3	4	5	9	7	8	6	10	11
<ul> <li>Cycle 1</li> <li>Charge (formation), AH</li> <li>0.86 amp to input or 2.1V 1st cell</li> <li>0.86 amp to 1.97V 1st cell (after seal)</li> <li>Total, AH</li> <li>AC Impedance before formation, mohms</li> <li>AC Impedance after cycle 3 charge, mohms</li> <li>Discharge, AH</li> <li>Cycle 2</li> <li>Charge, AH</li> <li>Step 1 @ .86 amp to 2.0V (1st cell)</li> <li>Step 2 @ .50 amp to 1.98V/cell</li> <li>Total, AH</li> </ul>	37.8 39.4 76 50 35.8 35.1 35.1 39.3	37.8 1.6 39.4 72 44 44 35.8 35.8 38.6	37.8 1.6 39.4 76 27 27 35.8 35.1 35.1	37.8 1.6 39.4 76 32 35.8 35.8 35.8	37.8 1.6 39.4 73 63 35.8 35.1	37.8 1.6 39.4 69 36 35.8 35.1 1.2 36.3	37.8 39.4 74 60 60 35.8 35.1 35.1	37.8 1.6 39.4 72 51 51 35.8 35.1 35.1	37.8 1.6 39.4 61 78 35.8 35.1 35.1 35.1	37.8 1.6 39.4 84 39 35.8 35.1 35.1 37.5	37.8 1.6 39.4 76 46 35.8 35.1 35.1
• Discharge, AH 6.4 amps to 1.30V/cell	39.6	39.6	38.4	39.0	39.9	39.0	39.2	39.5	40.0	39.4	37.8
Cycle 3  Charge Step 1 @ .86 amp to 2.0V (1st cell) Step 2 @ .50 amps to 1.98V/cell Total, AH	28.3 4.8 33.1	28.3 7.1 35.4	28.3 7.1 35.4	28.3 6.1 34.4	28.3 7.2 35.5	28.3 7.4 35.7	28.3 7.1 35.4	28.3 7.2 35.5	28.3 6.1 34.4	28.3 7.2 35.5	28.3 7.7 36.0

Cell nominal capacity based on .25 AH/gm silver. Cell electrolyte: 43% KOH 90% saturated with Zn0. Zn0 to silver weight ratio: 1.5:1 NOTES:

Table 13 (contd)

Plate Wrapped: Positive; Order of Separation, + to -: 1EM470, 4FSC; Nominal Capacity:	- to -: I	EM470,	4FSC;	Nomina	1 Capac	ity: 25	AH	
Test Parameter and Cell S/N	12	13	14	15	16	17	18	19
<ul> <li>Cycle 1</li> <li>Charge (formation), AH</li> <li>0.86 amp to input or 2.1 volts 1st cell</li> <li>0.86 amp to 1.97V 1st cell (after seal)</li> <li>Total, AH</li> <li>AC Impedance before formation, mohms</li> <li>AC Impedance after cycle 3 charge, mohms</li> <li>6.4 amps to 1.30V 1st cell</li> </ul>	37.8	37.8	37.8	37.8	37.8	37.8	37.8	37.8
	1.6	1.6	1.6	1.6	1.6	1.6	1.6	1.6
	39.4	39.4	39.4	39.4	39.4	39.4	39.4	39.4
	78	79	70	78	81	69	75	73
	30	41	36	23	24	20	27	20
	35.8	35.8	35.8	35.8	35.8	35.8	35.8	35.8
<ul> <li>Cycle 2</li> <li>Charge, AH</li> <li>Step 1 @ .86 amps to 2.0V (1st cell)</li> <li>Step 2 @ .50 amp to 1.98V/cell</li> <li>Total, AH</li> <li>Discharge, AH</li> <li>6.4 amps to 1.30V/cell</li> </ul>	35.1	35.1	35.1	35.1	35.1	35.1	35.1	35.1
	1.1	4.7	4.7	2.2	1.0	1.1	2.5	3.7
	36.2	39.8	39.8	37.3	36.1	36.2	37.6	38.8
	35.8	40.6	41.0	39.6	37.6	38.8	40.2	40.2
Cycle 3  • Charge Step 1 @ .86 amp to 2.0V (1st cell) Step 2 @ .50 amp to 1.98V/cell Total, AH	28.3	28.3	28.3	28.3	28.3	28.3	28.3	28.3
	7.0	7.2	7.4	7.9	7.5	7.5	7.6	7.3
	35.3	35.5	35.7	36.2	35.8	35.8	35.9	35.6

Cell nominal capacity based on .25 AH/gm silver. Cell electrolyte: 43% KOH 90% saturated with Zn0. Zn0 to silver weight ratio: 1.5:1 (3) (1) NOTES:

Table 14. Cycling performance of Phase II Design 3 cells

Plate Wrapped: Positive; Order of Separation,	+ to -: 1EM470, 2FSC; 4RAI; Cell Nominal Capacity:	EM470	, 2FSC;	4RAI;	Cell No	minal (	Japacity	7: 28 AH	Н	
Test Parameter and Cell S/N	23	24	25	97	27	28	59	30	31	32
Cycle 1  Charge (formation), AH  0.97 amp to input or 2.1V 1st cell	42.4	42.4	42.4	42.4	42.4	42.4	42.4	42.4	42.4	42.4
0.97 amp to 1.97V 1st cell (after seal)  Total, AH  AC Impedance before formation moluns  AC Impedance after cycle 3 charge, moluns	1.3 43.7 52 36	1. 5 43. 7 43 36	43.7 50 65	43.7 51 42	43.7 48 54	43.7 54 34	43.7 57 35	43.7 28	43.7 43.7 27	43.7 63 41
• Discharge, AH 7.2 amps to 1.30V 1st cell	39.4	39.4	39.4	39.4	39.4	39.4	39.4	39.4	39.4	39.4
Cycle 2			-							
• Charge, AH Step 1 @ 0.97 amp to 2.0V (1st cell) Step 2 @ 0.55 amp to 1.98V/cell	38.6	38.6	38.6	38.6	38.6	38.6	38.6	38.6	38.6	38.6
Total, AH	41.1	38.9	38.9	42.7	40.5	40.3	40.0	41.5	40.6	40.1
• Discharge, AH 7.2 amps to 1.30V/cell	38.1	38.2	35.8	41.6	37.9	38.9	37.8	39.9	38.1	37.2
Cycle 3										
• Charge Step 1 @ 0.97 amp to 2.0V (1st cell) Step 2 @ 0.55 amp to 1.98V/cell	36.8	36.8	35.0	36.8	36.8	36.8	36.8	36.8	36.8	36.8
Total, AH	37.8	37.7	37.2	39.3	38.0	39.8	39.4	38.7	40.0	38.6

Cell nominal capacity based on .25 AH/gm silver. Cell electrolyte: 43% KOH 90% saturated with Zn0. Zn0 to silver weight ratio: 1.5:1. 3(2) NOTES:

Table 14 (contd)

Plate Wrapped: Positive: Order of Separation, + to -:	+ to -	: 1EM4	70, 2FS	3C; 4RA	I; Cell	1EM470, 2FSC; 4RAI; Cell Nominal Capacity: 28 AH	1 Capac	ity: '28	AH
Test Parameter and Cell S/N	33	34	35	36	37	38	39	40	41
Cycle 1									
• Charge (formation), AH									
0.97 amp to 1.97V 1st cell	42.4	42.4	42.4	42.4	42.4	42.4	42.4	42.4	42.4
Total, AH	43.7	43.7	43.7	43.7	1.5	1.3	1.3		1.3
AC Impedance before formation, mohms	53	45	64	53	47.	47.	4.0.		43.7
<ul> <li>AC Impedance after cycle 3 charge, mohms</li> <li>Discharge, AH</li> </ul>	34	40	39	59	30	24	33		30
7.2 amps to 1.30V 1st cell	39.4	40.0	40.0	40.0	40.0	40.0	40.0	40.0	40.0
Cycle 2									
• Charge, AH								-	
Step 1 @ 0.97 amp to 2.0V (1st cell) Step 2 @ 0.55 amp to 1 98V/21	38.6	38.6	38.6	38.6	38.6	38.6	38.6	38.6	38.6
Total, AH	40.3	40.4	42.6	4.2	3.7	4.6	2.2	1.8	4.1
• Discharge, AH	)			) · [#	46.5	47.0	40.8	40.4	42.7
7.2 amps to 1.30V/cell	31.2	36.4	40.5	37.5	42.1	40.3	41.1	38.4	41.9
Cycle 3			-					-	_
• Charge								-	
Step 1 @ 0.97 amp to 2.0V (1st cell) Step 2 @ 0.55 amp to 1.98V/cell	36.8	36.8	36.8	36.8	36.8	36.8	31.5	31.5	31.5
Total, AH	38.9	37.7	39.5	39.0	39.9	37.7	35.5	38.8	32.9
									` ; ;

Cell nominal capacity based on 0.25 AH/gm silver. Cell electrolyte: 43% KOH 90% saturated with Zn0. Zn0 to silver weight ratio: 1.5:1 (3) NOTES:

Cycling performance of Phase II Design 4 cells Table 15.

Plate Wrapped: Negative; Order of Separation, + to -: Nominal Capacity; 31 AH	+ to -:	1EM47	61, 6RA	I; Cell	Pack P	1EM476I, 6RAI; Cell Pack Pressure:				
Test Parameter and Cell S/N	45	46	47	48	49	50	51	52	53	54
Cycle 1  Charge (formation), AH  1.08 amps to input or 2.1V 1st cell 1.08 amps to 1.97V 1st cell (after seal) Total, AH  AC Impedance before formation, mohms AC Impedance after cycle 3 charge, mohms Discharge, AH  8.0 amps to 1.30V 1st cell  Cycle 2  Charge, AH Step 1 @ 1.08 amps to 2.0V (1st cell) Step 2 @ .62 amp to 1.98V/cell Total, AH  Step 2 @ .62 amp to 1.98V/cell  B.0 amps to 1.30V/cell	41.2 7.4 48.6 43.6 48.5 48.9 49.3 46.6	41.2 7.4 48.6 44.5 53 49.4 1.2 50.6 48.0	41.2 7.4 48.6 35 38 48.5 48.9 0.8 49.7	41.2 7.4 48.6 35 48.5 49.4 47.8	41.2 7.4 48.6 53 48.5 48.9 0.4 49.3	41.2 7.4 48.6 32 32 48.5 48.9 0.9 49.8	41.2 7.4 48.6 40 43 48.5 49.4 2.6 52.0	41.2 7.4 488.6 488.6 49.4 49.4 52.8 48.5	41. 2 48. 6 34 34 45. 7 48. 9 0. 4 49. 3	41.2 48.6 49.6 43.7 45.7 45.9 45.9
Cycle 3  • Charge Step 1 @ 1.08 amps to 2.0V (1st cell) Step 2 @ .62 amps to 1.98V/cell Total, AH	33.6 4.5 38.1	33.6 9.2 42.8	33.6 9.2 42.8	34.2 7.2 41.4	35.4 9.2 44.6	35.4 9.2 44.6	33.7 5.9 39.6	32.7 3.0 35.7	32.7 7.2 39.9	32.3 3.7 36.4

Cell nominal capacity based on 0.25 AH/gm silver. Cell electrolyte: 43% KOH 90% saturated with Zn0. Zn0 to silver weight ratio: 1.5:1 NOTES:

Table 15 (contd)

	T		
	63	41.2 48.4 40 40 40 42.8 42.8 48.9 0.4 49.3 32.8	3.7
	62	41. 2 48. 4 40 47 42. 8 48. 9 60. 4 49. 3 35. 4	5.6
	61	41. 2 48. 4 34 42. 8 42. 8 60. 4 49. 3 32. 7	3.7
ressure	09	41.2 7.2 48.4 48.4 40.4 45.7 49.4 47.3	39.5
Pack P	59	41. 2 48. 4 36 38 45. 7 48. 9 0. 4 49. 3 46. 7	3.6
I; Cell	58	412 48.4 30 39 48.9 48.9 0.5 49.4 46.3	39.8
6I, 6RA	57	123 g 41. 2 7. 2 48. 4 38 45. 7 48. 9 1. 4 50. 3 45. 9	39.3
1EM47	56	41.2 48.4 32.7 45.7 49.4 1.4 48.4 48.4	35.7
+ to -:	55	41.2 48.4 42.4 47.7 45.7 48.9 0.4 49.3 46.6	5.4
Plate Wrapped: Negative; Order of Separation, + to -: 1EM4761, 6RAI; Cell Pack Pressure:	Test Parameter and Cell S/N	• Charge (formation), AH  1.08 amps to input or 2.1 volts 1st cell 1.08 amps to 1.97V 1st cell (after seal) Total, AH  • AC Impedance before formation, mohms • AC Impedance after cycle 3 charge, mohms Discharge, AH  8.0 amps to 1.30V 1st cell  Cycle 2  • Charge, AH  Step 1 @ 1.08 amps to 2.0V (1st cell) Step 2 @ .62 amps to 1.98V/cell Total, AH  8.0 amps to 1.30V/cell  Cycle 3  • Charge Step 1 @ 1.08 amps to 2.0V (1st cell)	

Cell nominal capacity based on 0.25 AH/gm silver. Cell electrolyte: 43% KOH 90% saturated with Zn0. Zn0 to silver weight ratio: 1.5:1 (3) (2) NOTES:

Table 16. Cycling performance of Phase II Design 5 cells

Plate Wrapped: Negative; Order of Separation, Cell Nominal Capacity: 28 AH	ration, + to -: 1EM470, 2FSC, 4RAI; 28 AH	1EM47	0, 2FSC	3, 4RAI							
Test Parameter and Cell S/N	29	89	69	10	71	72	73	74	75	92	77
<ul> <li>Cycle 1</li> <li>Charge (formation), AH</li> <li>97 amp to input or 2.1V 1st cell</li> <li>AC Impedance before formation mohms</li> <li>AC Impedance, after cycle 3 chg., mohms</li> <li>Discharge, AH</li> <li>7.2 amps to 1.30V 1st cell</li> </ul>	42. 2	42. 2	42. 2	42.2	42. 2	42.2	42. 2	42.2	42. 2	42.2	42. 2
	49	36	48	51	48	42	26	57	43	54	44
	42	49	82	66	44	60	58	54	58	44	84
	30. 7	30. 7	30. 7	30.7	30. 7	30.7	30. 7	30.7	30. 7	30.7	30. 7
Cycle 2  • Charge, AH Step 1 @ .97 amp to 2.0V (1st cell) Step 2 @ .55 amp to 1.98V/cell Total, AH • Discharge, AH 7.2 amps to 1.30V/cell	29.6	29.6	29.6	29.6	29.6	29.6	29.6	29.6	29.6	29.6	29.6
	4.4	5.5	4.7	4.4	4.7	5.9	3.0	4.4	3.0	4.4	4.4
	34.0	35.1	34.3	34.0	34.3	35.5	32.6	34.0	32.6	34.0	34.0
	42.6	42.1	41.1	41.1	42.8	39.8	39.8	37.2	39.8	42.8	42.6
Cycle 3  • Charge Step 1 @ .97 amp to 2.0V (1st cell) Step 2 @ .55 amp to 1.98V/cell Total, AH	30.6	30.6	30.6	30.6	30.6	30.6	30.6	30.6	30.6	30.6	30.6
	7.8	9.4	8.6	6.9	8.3	6.0	11.7	3.5	6.8	5.6	6.8
	38.4	40.0	39.2	37.5	38.9	36.6	42.3	34.1	37.4	36.2	37.4

Cell nominal capacity based on 0.25 AH/gm silver. Cell electrolyte: 43% KOH 90% saturated with Zn0. Zn0 to silver weight ratio: 1.5:1. 3(2) NOTES:

Table 16 (contd)

Plate Wrapped: Negative; Order of Separation, + to -: 1EM470, 2FSC, 4RAI; Cell Pack Pressure: 40 oz/in <sup>2</sup> ; Cell Nominal Capacity: 28 AH	+ to -: ninal Ca	1EM47	70, 2FS	C, 4RA	[; Cell ]	Pack		
Test Parameter and Cell S/N	78	62	80	81	82	83	84	85
<ul> <li>Cycle 1</li> <li>Charge (formation), AH</li> <li>0.97 amp to input or 2.1V 1st cell</li> <li>AC Impedance before formation mohms</li> <li>AC Impedance after cycle 3 chg., mohms</li> <li>7.2 amps to 1.30V 1st cell</li> </ul>	42. 2	42. 2	42. 2	42.2	42. 2	42.2	42.2	42.2
	44	32	49	55	68	54	63	60
	67	32	43	75	58	51	63	52
	30. 7	30. 7	30. 7	30.7	30. 7	30.7	30.7	30.7
• Charge, AH Step 1 @ .97 amp to 2.0V (1st cell) Step 2 @ .55 amp to 1.98V/cell Total, AH • Discharge, AH 7.2 amps to 1.30V/cell	29.6	29.6	29.6	29.6	29.6	29.6	29.6	29.6
	4.1	4.4	4.1	4.1	4.4	5.6	3.0	4.4
	33.7	34.0	34.0	33.7	34.0	35.2	32.6	34.0
	38.5	31.8	43.0	42.1	42.6	42.3	42.5	42.4
Cycle 3  • Charge Step 1 @ . 97 amp to 2. 0V (1st cell) Step 2 @ . 55 amp to 1. 98V/cell Total, AH	30.6	30.6	30.6	30.6	30.6	30.6	30.6	30.6
	6.0	6.0	7.8	10.0	7.8	7.8	10.0	6.0
	36.5	36.6	38.3	40.5	38.3	38.3	40.5	36.5

 Cell nominal capacity based on 0.25 AH/gm silver.
 Cell electrolyte: 43% KOH 90% saturated with Zn0.
 Zn0 to silver weight ratio: 1.5:1. NOTES:

Table 17. Cycling performance of Phase II Design 6 cells

Step 1 @ .97 amps to 2.0V (1st cell) 31.4 31.4 31.4 31.4 31.4 31.4 31.4 31.4	
78 27 24 66 69	31.4   31.4   31.4   31.4   31.4   31.4
77.000	7.8 5.2 5.6 6.6 5.6 6.9

Cell nominal capacity based on 0.25 AH/gm silver. Cell electrolyte: 43% KOH 90% saturated with Zn0. Zn0 to silver weight ratio: 1.5:1. 3(2)(2) NOTES:

Table 17 (contd)

Plate Wrapped: Both; Order of Separation, + to -: 1EM4761, 3RAI, 1EM476I, 4RAI; Cell Nominal Capacity: 28 AH	o -: 1EN	44761, 3	RAI, 1	EM4761	, 4RAI;				
Test Parameter and Cell S/N	66	100	101	102	103	104	105	106	107
<ul> <li>Cycle 1</li> <li>Charge (formation), AH</li> <li>97 amp to input or 2.1V 1st cell</li> <li>97 amp to 1.97V 1st cell (after seal)</li> <li>Total, AH</li> <li>AC Impedance before formation, mohms</li> <li>AC Impedance after cycle 3 charge, mohms</li> <li>Discharge, AH</li> <li>7.2 amps to 1.30V 1st cell</li> <li>Cycle 2</li> <li>Charge, AH</li> <li>Step 1 @ .97 amp to 2.0V (1st cell)</li> <li>Step 2 @ .55 amp to 1.98V/cell</li> <li>Total, AH</li> </ul>	39.3 45.6 38 47 41.6 48.5 41.2	39.3 6.3 45.6 41.6 47.6 3.3 50.9	39.3 6.3 45.6 24 52 41.6 47.6 51.4 43.8	39.3 6.3 45.6 23 41.6 47.6 51.2 44.0	39.3 6.3 45.6 37 35 41.6 47.6 3.3 50.9	39.3 6.3 45.6 50 41.6 47.6 51.2 41.5	39.3 6.3 45.6 42 41.6 47.6 3.3 50.9	39.3 45.6 41.6 47.6 48.5 39.0	39.3 6.3 45.6 43.2 47.6 50.0 43.2
Cycle 3  • Charge Step 1 @ .97 amp to 2.0V (1st cell) Step 2 @ .55 amp to 1.98V/cell Total, AH	31.4 8.1 39.5	31.4 9.3 40.7	31.4 6.6 38.0	31.4 5.6 37.0	31.4 5.6 37.0	31.4 6.9 38.3	31.4 6.6 38.0	31.4 7.5 38.9	31.4 4.8 36.2

Cell nominal capacity based on 0.25 AH/gm silver. Cell electrolyte: 43% KOH 90% saturated with Zn0. Zn0 to silver weight ratio: 1.5:1. (1) NOTES:

Table 18. Cycling performance of Phase II Design 7 cells

Plate Wrapped: Positive; Order of Separation, + to -: 1EM470, 4RAI2291, 2FSC; Cell nominal capacity: 28 AH	+ to -:	1EM47	0, 4RA]	.2291, 2	FSC;					
Test Parameter and Cell S/N	111	112	113	114	115	116	117	118	119	120
1 —	40.6	40.6	40.6	40.6	40.6	40.6	40.6	40.6	40.6	40.6
0.97 amp top-off charge to 1.97V 1st cell (sealed) Total Inmit	5.1	5.1		5.1	5.1	5.1	5.1	5.1	5.1	5.1
AC Impedance before formation, mohms AC Impedance after cycle 3 charge Discharge, AH	57 84	56 25	62 40	52 24	45 45 28	44 42 5	45 25	44 92	43 90	47 14
7.2 amps to 1.30V 1st cell Cycle 2	44.0	44.0	44.0	44.0	44.0	44.0	44.0	44.0	44.0	44.0
Charge, AH Step I @ 0.97 amp to 2.00V 1st cell Step II @ 0.6 amp to 1.98V/cell	29.6	29.6	29.6	29.6	29.6	29.6	29.6	29.6	29.6 10.2	29.6 5.8
Total Discharge, AH 7.2 amps to 1.30V/cell	38.6	36.5	38.3	37.8	29.1 39.0	39.8	37.8	36.7	39.8	35.4 35.6
Cycle 3  • Charge, AH  Step I @ 0.97 amp to 2.00V 1st cell  Step II @ 0.6 amp to 1.98V/cell  Total	34.7 1.5 36.2	34.7 2.1 36.8	34.7 2.9 37.6	34.7 0.2 34.9	34.7 0.9 35.6	34.7 2.9 37.6	34.7 1.5 36.2	29.9 1.0 30.9	29.9 9.1 39.0	29.9 1.4 31.3

£ (2) (£) NOTES:

Cell nominal capacity based on 0.25 AH/gram silver. Cell electrolyte: 43% KOH 90% saturated with Zn0. Zn0 to silver weight ratio: 1.5:1. Date of activation; 10/31/69 - Date on charged stand: 11/26/69.

Table 18 (contd)

Plate Wrapped: Positive; Order of Separation, + to -: 1EM470, 4RAI2291, 2FSC; Cell Nominal Capacity: 28 AH	+ to -:	1EM47	'0, 4RA	12291,	FSC;					
Test Parameter and Cell S/N	121	122	123	124	125	126	127	128	129	$\overline{\mathbf{x}}_{19}$
Cycle 1  Charge (formation), AH										
0.97 amp to input or 2.1V 1st cell 0.97 amp top-off charge (sealed)	40.6	40.6	5.1	40.6	40.6	40.6	40.6	40.6	45.1	l ! l 1
<ul> <li>Iotal Input</li> <li>AC Impedance before formation, mohms</li> <li>AC Impedance after cycle 3 charge</li> </ul>	45.7 62 78	45.7 51 28	45.7 54 90	45.7 45 31	45.7 44 72	45.7 49 44	45.7 53 48	45.7 49 20	45.7 45 22	45.7 50 47
• Discharge, AH 7.2 amps to 1.30V 1st cell	44.0	44.0	44.0	44.0	44.0	44.0	44.0	44.0	44.0	44.0
Cycle 2										
• Charge, AH Step I @ 0.97 amp to 2.00V 1st cell Step II @ 0.6 amp to 1.98V/cell	29.6	29.6	29.6	29.6	29.6	29.6	29.6	29.6	29.6	29.6
Total  Discharge AH	41.3	37.5	41.5	38.0	37.8	41.1	39.0	40.7	39.0	38.7
7.2 amps to 1.30V/cell	41.0	38.8	41.6	38.8	39.0	41.1	38.4	39.1	37.9	38.7
Cycle 3				-						
• Charge, AH Step I @ 0.97 amp to 2.00V 1st cell Step II @ 0.6 amp to 1.98V/cell	29.9	29.9	29.9	30.3	30.3	30.3	30.3	30.3	30.3	31.8
Total	39.5	41.4	41.4	36.1	39.0	40.1	37.7	37.5	37.1	37.2

Cell nominal capacity based on 0.25 AH/gram silver.
Cell electrolyte: 43% KOH 90% saturated with Zn0.
Zn0 to silver weight ratio: 1.5:1.
Date of activation: 10/31/69 - Date on charged stand: 11/26/69. £ (2) (£) NOTES:

Phase II cycles 1 through 3 performance mean values Table 19.

Design Number	2	6,	4	5	9	7
Plate Wrapped	+	+	ı	ı	Both	+
Order of Separation, + to -	1EM470 4FSC	1EM470 2FSC 4RAI	1EM476I 6RAI	1EM470 2FSC 4RAI	1EM476I 3RAI 1EM476I 4RAI	1EM470 4RAI 2FSC
Cell Nominal Capacity, AH	25	28	31	28	28	28
Cell S/N	1 thru 19	23 thru 41	45 thru 63	67 thru 85	89 thru 107	111 thru 129
<ul> <li>Cycle 1</li> <li>Charge (formation, AH)</li> <li>7 ma/in² to input or 2.1V 1st cell</li> <li>7 ma/in² to 1.97V 1st cell after seal</li> <li>Total AH</li> <li>AC Impedance, Before Formation, mohms</li> <li>AC Impedance, After Cycle 3 Charge, mohms</li> </ul>	37.8 1.6 39.4 74	42.4 1.3 43.7 50 38	41.2 7.3 48.5 38	42.2  42.2 57	39.3 6.3 45.6 47	40.6-45.1 5.1-0.6 45.7 50 47
<ul> <li>Discharge, AH</li> <li>52 ma/in<sup>2</sup> to 1.30V 1st cell</li> <li>Mid Voltage during Discharge, Volts</li> </ul>	35.8 1.52-1.53	39.6 1.48-1.51	46.4 1.50	30.7 1.46-1.50	40.3 1.48-1.50	44.0 1.50-1.51
<ul> <li>Cycle 2</li> <li>Charge, AH</li> <li>Step 1 to 2.0V 1st cell</li> <li>Step 2 to 1.98V/cell</li> <li>Total AH</li> <li>Discharge, AH</li> <li>52 ma/in² to 1.30V/cell</li> <li>Mid Voltage during Discharge, Volts</li> </ul>	35.1 2.6 37.7 39.2 1.50-1.52	38.6 2.3 40.9 38.6 1.49	49.0 1.0 50.0 47.6 1.48-1.50	29.6 4.4 34.0 40.9 1.48-1.50	47.6 2.2 49.8 42.2 1.46-1.50	29.6 9.1 38.7 38.7 38.7 1.49-1.50
Cycle 3  Charge, AH Step 1 to 2.0V 1st cell Step 2 to 1.98V/cell Total AH	28.3 7.1 35.4	35.9 2.3 38.2	33.5 39.9	30.6 7.5 38.1	31.4 7.0 38.4	31.8 5.4 37.2
Discharge Current, amps (52 ma/in <sup>2</sup> ) Charge Current, amps Step 1 (7 ma/in <sup>2</sup> ) Step 2 (4 ma/in <sup>2</sup> )	6.4 0.86 0.50	7.2 0.97 0.55	8.0 1.08 0.62	7.2 0.97 0.55	7.2 0.97 0.55	7.2 0.97 0.60

Table 20. Phase II limiting cells on capacity check cycles

					CELL S/N	N/S				
5	11	11	24	8	12	12	8	6	11	11
3	24 32 34	34	34	34	25 84					
4	46 47	25	57 (52)							
5	74	74	74	74	74 90					
9	86	102	92 (39)							
7	115	112	112	128	128 (99)					
DESIGN	0	25	50	75	100	125	150	175	200	225
GROUP					CYCLE NUMBER	UMBER				

(n) = CYCLE NUMBER WHEN 1st CELL FAILED TO DELIVER 50% DOD

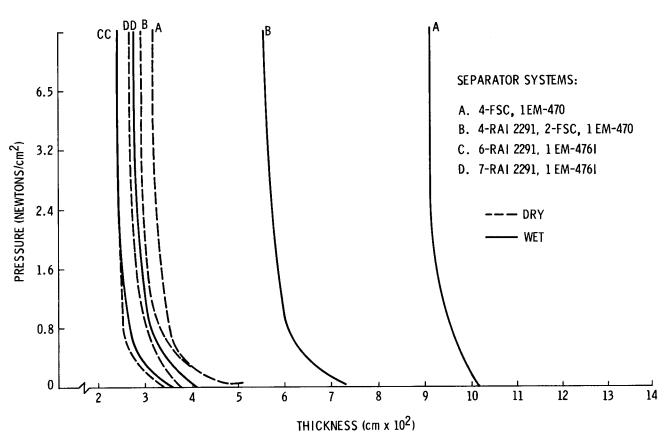


Fig. 1. Effect of pressure on separator system thickness

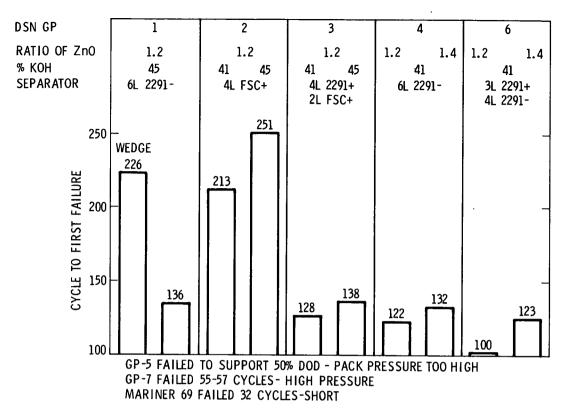


Fig. 2. Phase I cycle results (to first cell failure)

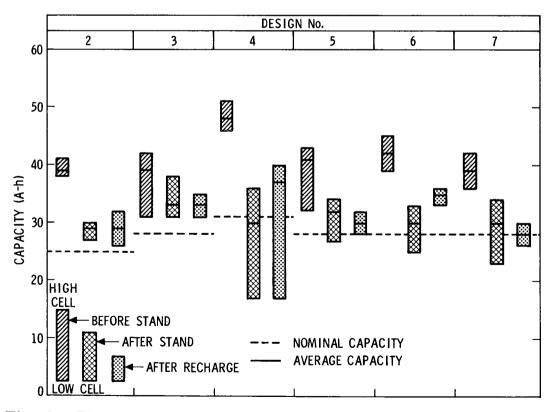


Fig. 3. Phase II cell capacity check results before and after stand

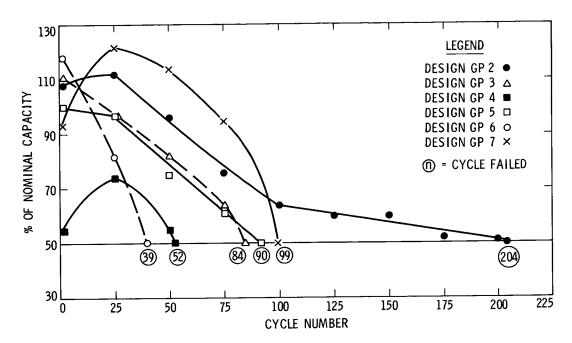


Fig. 4. Phase II capacity available during 50% DOD cycles, measured on lowest cell in battery (19 cell battery)

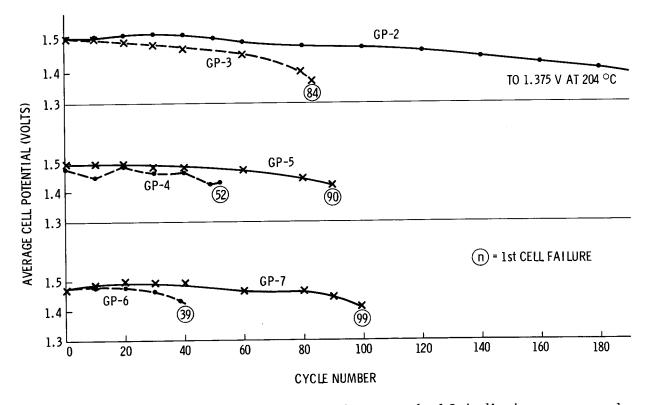


Fig. 5. Average cell potential of batteries at end of 2-h discharge on cycle test to first cell failure; discharge rate C/4!

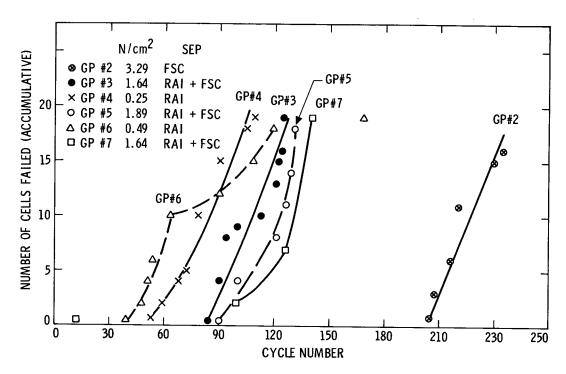


Fig. 6. Phase II failure rate during 50% DOD cycles